



SUPPLEMENTARY MATERIAL TO

**The influence of glass fibers on the morphology of  $\beta$ -nucleated isotactic polypropylene evaluated by differential scanning calorimetry**

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J. Serb. Chem. Soc. 80 (2) (2015) 223–235

THEORETICAL BACKGROUND

From the DSC scans (isothermal crystallization at given  $T_c$  and then melting of the crystallized sample), the equilibrium melting temperature ( $T_m^0$ ) was determined by the Hoffmann–Weeks method:<sup>1</sup>

$$T'_m = \frac{T_m^0(\gamma-1)}{\gamma} + \frac{T_c}{\gamma} \quad (1)$$

where  $\gamma$  is a constant that represents the ratio between the final thickness of the crystalline lamellae and the initial critical thickness, and  $T'_m$  is the observed melting temperature of the sample isothermally crystallized at  $T_c$ . According to the kinetic theory of polymer crystallization,<sup>2</sup> assuming that the growth of lamellae is controlled by a process of secondary nucleation, the temperature dependence of the overall kinetic constant,  $k$ , is given by the Eq. (2):

$$\frac{\log(k)}{n} = A_0 - \frac{\Delta F^*}{2.3RT_c} - \frac{\Delta\Phi^*}{2.3KT_c} \quad (2)$$

where  $A_0$  is a constant (assuming that the primary nucleation density at each  $T_c$  examined does not vary with time),  $\Delta F^*$  is the activation energy for the transport of crystallizing units across the liquid–solid interface,  $K$  is the Boltzmann constant,  $n$  is the Avrami exponent, and  $\Delta\Phi^*$  is the energy of formation of a nucleus with critical dimensions, expressed by Eq. (3):<sup>2</sup>

$$\Delta\Phi^* = \frac{4b_0\sigma\sigma_e T_m}{\Delta_{\text{melt}}H\Delta T} \quad (3)$$

where  $b_0$  is the molecular thickness, and  $\sigma$  and  $\sigma_e$  are the crystal growth lateral surface energy and the crystal fold surface energy, respectively.  $\Delta_{\text{fus}}H$  is the enthalpy of fusion and

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$\Delta T = T_m^0 - T_c$  is the supercooling.  $\Delta F^*$  is usually expressed as the activation energy of viscous flow given by the Williams–Landel–Ferry relation, Eq. (4):<sup>3</sup>

$$\Delta F^* = \frac{C_1 T_c}{(C_2 + T_c - T_g)} \quad (4)$$

where  $C_1$  and  $C_2$  are constants ( $C_1 = 17.2 \text{ kJ mol}^{-1}$ ;  $C_2 = 51.5 \text{ K}$ ) and  $T_g$  is the glass transition temperature. In further calculations, the literature value of  $T_g = 260 \text{ K}$  was used for iPP.<sup>4</sup> The plot of:  $[\log k/n + \Delta F^*/2.3RT_c]$  vs.  $T_m'/T_c\Delta T$  yields a straight line with a negative slope equal to:

$$\frac{4b_0\sigma\sigma_e}{2.3K\Delta_{\text{fus}}H} \quad (5)$$

from which  $\Delta F^*$  and  $\sigma_e$  are obtained assuming that  $b_0 = 0.525 \text{ nm}^5$  and  $\Delta_{\text{fus}}H$  of 193 and 209  $\text{J g}^{-1}$ , and  $\sigma = 0.1b_0\Delta_{\text{fus}}H$ .

To calculate the nucleation activity ( $\theta$ ) of foreign additives and substrates during the crystallization of a polymer melt, a method was proposed by Dobreva *et al.*<sup>6</sup> for analyzing DSC data.  $\theta$  is defined as:

$$\theta = \frac{A_{k3}^*}{A_{k3}^0} \quad (6)$$

where

$$A_{k3}^0 = \frac{16\pi\sigma V_m^2}{3\Delta_{\text{melt}}S^2\Delta T_p^2} \quad (7)$$

is the work of homogeneous nucleation, in which  $V_m$  is molar volume of the crystallizing substance,  $\Delta_{\text{melt}}S$  is entropy of melting and  $\Delta T_p = T_m^0 - T_{c\max}$  (where  $T_{c\max}$  corresponds to the crystallization peak temperature in the nonisothermal regime), and  $A_{k3}^*$  is the work of heterogeneous nucleation. Clearly,  $\theta$  is unity for absolutely inert substrates and is practically zero for very active substrates. Following the formalism presented by Dobreva *et al.*,<sup>6</sup> the Avrami equation<sup>7</sup> (8):

$$\alpha = 1 - \exp(-kt^n) \quad (8)$$

for nonisothermal conditions can be transformed into:

$$\log(V_c) = \text{const} - \frac{B^0}{2.3\Delta T_p^2} \quad (9)$$

where

$$B^0 = \frac{16\pi\sigma V_m^2}{3T_m^0\Delta_{\text{melt}}S^2} \quad (10)$$

and where  $V_c$  is the cooling rate. The activity of a substrate,  $\theta$ , is then given by the ratio of the two slopes  $B^*$  and  $B_0$ .

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